Quantum Mechanical & Electromagnetic Systems Modelling Lab

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Accurate Characterization of Radiation from Interconnects on Interposer at mmWave Frequencies

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Outline

Introduction

Design test vehicles

Design measurement set-up

Measurement results

Conclusions & future work







Towards mmWave communication



Driverless cars



Smart cities







Bandwidth ↑



Next-generation communication standard





mmWave frequencies

Interposer to achieve heterogeneous systems





Radiated emission

Proximity of different components & mmWave operation

- $\rightarrow\,$ Stringent electromagnetic compatibility (EMC) requirements to guarantee proper performance
- Signal integrity high-speed lines need to be preserved through entire, complex routing
- \blacktriangleright Rising frequencies \rightarrow electric length $\uparrow \rightarrow$ lines become effective radiators
- Composite nature interposer makes identification noise sources almost impossible



Goal

Study into radiation mechanism of interposers at mmWave frequencies

- Accurate measurements through well-designed set-up
 - \rightarrow Particular care in shielding influence measurement equipment
- Designated interposer structures with corresponding simulation model
- Simulation study into mechanism responsible for discrepancy between measurement ↔ model



Design test vehicles

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Interposer

Patch antenna



All dimensions in mm

- $\blacktriangleright \ \ Strong \ radiator \rightarrow calibration \ \ structure$
- Easy detection fabrication deviation







Interposer

Interconnects



HL972LF(LD) c_{u} $15 \mu m$ HL972LF(LD): $\epsilon_{r} = 3.4$, tan $\delta = 0.004$



- Archetypal microstrip interconnects
- $\blacktriangleright\,$ Two variants: top via shorted or matched to 50 $\Omega\,$



Measurement PCB

Design & rationale



PCB measures 6.5 cm by 4 cm

- Accommodates connector and fixes interposer to measurement system
- Feed line at the back to minimize forward radiation



 $\epsilon_r = 3.6$, tan $\delta = 0.004$



Design measurement set-up



Anechoic chamber

Specifications



Spherical measurement system in full anechoic mode

Calibration



WR-34 Probe

standard gain horn

Losses GCPW line PCB calibrated via dedicated TRL set



Anechoic chamber

Shielding





Anechoic chamber

Shielding



- Right-angled adapter right at the connector to avoid long cable in the plane of the interposer
- Cable wrapped in RF absorbent foam for additional shielding
- Pyramidal absorbers at the back of the PCB to avoid unwanted reflections



Measurement results

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Patch antenna

Measurement vs. simulation model



- Realized gain in the $\phi = 90^{\circ}$ cut at 28 GHz
- Interposer only model exhibits typical radiation pattern patch antenna
- Measured pattern has broadened beam and suppressed back radiation due to PCB and ...
- together with the full model (interposer + PCB) exhibits a prominent, superimposed ripple
- → Origin turns out to be *surface waves* originating on the interposer, interacting with the PCB's ground plane



Surface waves

Main characteristics

- Surface waves or (Sommerfeld-)Zenneck waves are cylindrical waves supported by interfaces of media with different e
- ► Decay slower (∝ 1/√r) than space-waves (∝ 1/r) in the propagation direction but decay exponentially along their normal axis
- Classified in typical waveguide modes: transverse electric (TE) and magnetic (TM) modes
 - Interposer only supports TM0 mode at 30 GHz







Surface waves



simplified model: interposer backed by PEC ground plane with PCB's dimensions



- Neither the interposer model nor one backed by an infinite ground plane, show any ripple
- However, a simplified model does give rise to the observed phenomenon
- $\rightarrow\,$ Surface waves originate on interposer and interact with electrically large ground plane PCB



Surface waves

Interconnect structures



- Realized gain in the φ = 90° cut at 28 GHz for a shorted straight line
- Ripple does occur for weak radiators in measurement, full and simplified model but not in the interposer model, further demonstrating its origin



Maximum electric field strength

Patch antenna

In an EMC context, a more relevant quantity than the gain is the maximum electric field strength at a fixed input power and distance. Does the ripple have an effect on such measure?



Seemingly not for the patch antenna:

- Measurement, full & interposer model agree very well
- Simplified model lacks losses
- → Ripple compensates for gain reduction due to ground plane



Maximum electric field strength





- Interposer model underestimates max. measured field by up to 6 dB
- Full and simplified predict very similar levels
- → Ripple has larger impact on microstrip line than on the patch antenna

Maximum electric field strength



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- Measurements exhibit unidentified dip in radiation
 - No decisive cause found
 - Presumably an unidentified mismatch issue
- Full and simplified predict very similar levels
- Difference with interposer model is a consistent 2-3 dB
- → Ripple has larger impact on microstrip line than on the patch antenna

Conclusions & future work

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Conclusions

Five mmWave test vehicles to identify dominant radiation sources

Dedicated measurement set-up to prevent perturbation by external factors

Combined simulation and measurement strategy is able to predict maximum field levels accurately ...

... and reveals issue of interposer's surface waves interfering with PCB to (negatively) impact emission performance



Future work

Investigate (cost-effective) strategies to eliminate excitation surface waves

Explore design of vertical via topologies and other interconnect approaches to assess radiated emission

Realize, model and measure differential interconnects to assess common mode vs. differential mode performance





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